CONVERSION TABLE FOR U.S. AND METRIC SYSTEM

| METRIC TO U.S. |  | TO OBTAIN |
| :--- | :--- | :--- |
| MULTIPLY | $\times .03937$ | $=$ inches |
| millimeter (mm) | $\times .3937$ | $=$ inches |
| centimeters (cm) | $\times 39.37$ | $=$ inches |
| meters (m) | $\times 3.281$ | $=$ feet |
| meters (m) | $\times 1.094$ | $=$ yards |
| meters (m) | $\times .6214$ | $=$ miles |
| kilometers (km) | $\times 1093.62$ | $=$ yards |
| kilometers (km) | $\times 3280.87$ | $=$ feet |
| kilometers (km) | $\times 1.0567$ | $=$ quarts |
| liters (I) | $\times .2642$ | $=$ gallons |
| liters (I) | $\times .455$ | $=$ pounds |
| liters (I) | $\left({ }^{\circ} \mathrm{C} \times 1.80\right)+32^{\circ}$ | $=$ temp. in ${ }^{\circ} \mathrm{F}$ |
| temperature in ${ }^{\circ} \mathrm{C}$ | $\times 14.223$ | $=\mathrm{lb} / \mathrm{sq}$ in (PSI) |
| kilograms $/ \mathrm{cubic} \mathrm{centimeter}\left(\mathrm{kg} / \mathrm{cm}^{2}\right)$ | $\times 28.316$ | $=$ liters |
| cubic feet $(\mathrm{cu} \mathrm{ft)}$ |  |  |


| U.S. TO METRIC |  |  |
| :--- | :--- | :--- |
| MULTIPLY | $\times 25.4$ | TO OBTAIN |
| inches (in) | $\times 2.54$ | $=$ millimeters |
| inches (in) | $\times .254$ | $=$ meters |
| inches (in) | $\times .3048$ | $=$ meters |
| feet (ft) | $\times .9144$ | $=$ meters |
| yards (yds) | $\times 1.6093$ | $=$ kilometers |
| miles (mi) | $\times .0001943$ | $=$ kilometers |
| yards (yds) | $\times .0003048$ | $=$ kilometers |
| feet (ft) | $\times .945$ | $=$ liters |
| quarts (qts) | $\times 3.78$ | $=$ liters |
| gallons (gals) | $\times 2.2$ | $=$ liters |
| pounds (lbs) | $\left({ }^{\circ} \mathrm{F}-32\right) \times .5556$ | $=$ temp. in ${ }^{\circ} \mathrm{C}$ |
| temperature in ${ }^{\circ} \mathrm{F}$ |  |  |
|  |  |  |
|  |  |  |

## MISCELLANEOUS CONVERSION FACTORS

| MULTIPLY |  | TO OBTAIN |
| :---: | :---: | :---: |
| AREA |  |  |
| acres (ac) | $\times 43560$ | = square feet |
| acres (ac) | $\times 4046.8$ | = square meters |
| square meters (sq m) | $\times 10.764$ | = square feet |
| square feet ( sq ft ) | $\times 144$ | = square inches |
| square inches (sq in) | $\times 6.452$ | = square centimeters |
| hectares (ha) | $\times 10000$ | = square meters |
| hectares (ha) | $\times 2.471$ | = acres |
| POWER |  |  |
| kilowatts (kW) | x 1.341 | = horsepower |
| FLOW |  |  |
| cubic feet/minute (cu ft/min) | x . 0004719 | = cubic meters/second |
| cubic feet/second (cu ft/sec) | x 02832 | = cubic meters/second |
| cubic yards/minute (cu yd/min) | x . 01274 | = cubic meters/second |
| gallons/minute (gal/min) | x . 22716 | = cubic meters/hour |
| gallons/minute (gal/min) | + 3.7854 | $=$ liters/minute |
| gallons/minute (gal/min) | $\times .06309$ | $=$ liters/second |
| cubic meters/hour (cu m/hr) | x 16.645 | = liters/minute |
| cubic meters/hour (cu m/hr) | x . 2774 | $=$ liters/second |
| liters/minute (1/min) | $\times 60$ | $=$ liters/second |
| VELOCITY |  |  |
| feet/second (ft/sec) | x. 3048 | = meters/second |


| MULTIPLY |  | TO OBTAIN |
| :--- | :--- | :--- |
| LENGTH | $\times 12$ | $=$ inches |
| feet (ft) | $\times .6214$ | $=$ miles |
| kilometers (km) | $\times 5280$ | $=$ feet |
| miles (mi) | $\times 1609.34$ | $=$ meters |
| miles (mi) | $\times .03937$ | $=$ inches |
| millimeters (mm) | $\times 6.89476$ | $=$ kilopascals |
| PRESSURE | $\times .068948$ | $=$ bars |
| PSI | $\times 100$ | $=$ kilopascals |
| PSI | $\times 2.31$ | $=$ feet of head |
| bars | $\times 7.48$ | $=$ gallons |
| PSI | $\times 28.32$ | $=$ liters |
| VOLUME | $\times 35.31$ | $=$ cubic feet |
| cubic feet (cu ft) | $\times 1.3087$ | $=$ cubic yards |
| cubic feet (cu ft) | $\times 27$ | $=$ cubic feet |
| cubic meters (cu m) | $\times 202$ | $=$ gallons |
| cubic meters (cu m) | $\times 43,560$ | $=$ cubic feet |
| cubic yards (cu yd) | $\times .003785$ | $=$ cubic meters |
| cubic yards (cu yd) | $\times 3.785$ | $=$ liters |
| acres/feet (ac/ft) | $\times 1.833$ | $=$ gallons |
| gallons (gal) |  |  |
| gallons (gal) |  |  |
| imperial gallons (ig) |  |  |

## SURGE PRESSURE

## $\mathrm{P}=\left(\frac{\mathrm{VL}_{\mathrm{L}}}{\mathrm{T}}\right)$ <br> WHERE: <br> $\mathbf{P}=$ Pressure rise (PSI) above the static pressure <br> $\mathbf{V}=$ Velocity of flow (ft/sec) <br> $\mathbf{L}=$ Length of pipe (ft) on the pressure side of the valve <br> $\mathbf{T}=$ Closing time of valve (sec) <br> CONVERSION TABLE FOR U.S. AND METRIC SYSTEM

Pressure drop calculations can be made for valves and strainers for different fluids, flow rates and sizes using the CV values and the following equation:

| $\mathbf{P}=\frac{(\mathrm{G})^{2} \text { (specific gravity liquid) }}{\left(\text { (CV Factor) }{ }^{2}\right.}$ |
| :--- |
| WHERE: |
| $\mathbf{P}=$ Pressure drop in PSI; feet of water $=\frac{\mathrm{PSI}}{.4332}$ |
| $\mathbf{C}=$ Gallons per minute |
| $\mathbf{C V}=$ Gallons per minute per 1 PSI pressure drop |

## WATER PRESSURE

| Water pressure varies by . 433 PSI for each foot of elevation <br> change, or about 1 PSI for every $\mathbf{2 . 3}$ ft. gained or lost. |
| :--- |
| DEFINITIONS |
| Static Pressure - Water pressure without movement |
| Dynamic Pressure - Water pressure with movement |
| Precipitation Rate - How fast water is applied to the soil |
| Transpiration Rate - Amount of water plants require to live |

Transpiration Rate - Amount of water plants require to live

## TYPICAL SOLENOID DHM READINGS

| Irritrol | 24 |
| :--- | :---: |
| Hunter | 24 |
| Rain Bird PGA | 36 |
| Rain Bird DV | 40 |
| Weathermatic | 30 |
| Toro 252 | 29 |
| Toro 1" | 53 |

## Where:

## G = Gallons per minute

CV = Gallons per minute per 1 PSI pressure drop

## FRICTION LOSS THROUGH FITTINGS

Friction loss through fittings is expressed in equivalent feet of the same pipe size and schedule for the system flow rate.
Schedule 40 head loss per 100 -feet values are usually used for other wall thicknesses and standard iron pipe size outside diameters.

| ITEM | 1/2" | 3/4" | 11 | 1-3/4" | 1-1/2" | 2" | 2-1/2" | 3" | 4" | 6" | 8" | 10" | 12" | 14" | 16" | 18" | 20" | 24" |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Tee Run | 1.0 | 1.4 | 1.7 | 2.3 | 2.7 | 4.0 | 4.9 | 6.1 | 7.9 | 12.3 | 14.0 | 17.5 | 20.0 | 25.0 | 27.0 | 32.0 | 35.0 | 42.0 |
| Tee Branch | 3.8 | 4.9 | 6.0 | 7.3 | 8.4 | 12.0 | 14.7 | 16.4 | 22.0 | 32.7 | 49.0 | 57.0 | 67.0 | 78.0 | 88.0 | 107.0 | 118.0 | 137.0 |
| 90 Ell | 1.5 | 2.0 | 2.5 | 3.8 | 4.0 | 5.7 | 6.9 | 7.9 | 11.4 | 16.7 | 21.0 | 26.0 | 32.0 | 37.0 | 43.0 | 53.0 | 58.0 | 67.0 |
| 45 Ell | . 8 | 1.1 | 1.4 | 1.8 | 2.1 | 2.6 | 3.1 | 4.0 | 5.1 | 8.0 | 10.6 | 13.5 | 15.5 | 18.0 | 20.0 | 23.0 | 25.0 | 30.0 |

## LIGHTING WIRE GAUGE CHART

|  | WATTS |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| FEET | 20 | 40 | 60 | 80 | 100 | 120 | 140 | 160 | 180 | 200 | 220 | 240 | 260 | 280 |
| 20 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 10 | 10 | 10 | 8 | 8 |
| 40 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 10 | 10 | 10 | 10 | 8 | 8 |
| 60 | 12 | 12 | 12 | 12 | 12 | 12 | 12 | 10 | 10 | 10 | 10 | 10 | 8 | 8 |
| 80 | 12 | 12 | 12 | 12 | 12 | 12 | 10 | 10 | 10 | 10 | 8 | 8 | 8 | 8 |
| 100 | 12 | 12 | 12 | 12 | 12 | 10 | 10 | 10 | 10 | 8 | 8 | 8 | 8 |  |
| 120 | 12 | 12 | 12 | 12 | 10 | 10 | 10 | 8 | 8 | 8 | 8 | 8 |  |  |
| 140 | 12 | 12 | 12 | 10 | 10 | 10 | 10 | 8 | 8 | 8 | 8 |  |  |  |
| 160 | 12 | 12 | 10 | 10 | 10 | 8 | 8 | 8 | 8 |  |  |  |  |  |
| 180 | 12 | 10 | 10 | 10 | 8 | 8 | 8 | 8 |  |  |  |  |  |  |
| 200 | 10 | 10 | 10 | 10 | 8 | 8 | 8 |  |  |  |  |  |  |  |
| 220 | 10 | 10 | 10 | 8 | 8 | 8 |  |  |  |  |  |  |  |  |
| 240 | 10 | 10 | 10 | 8 | 8 | 8 |  |  |  |  |  |  |  |  |
| 260 | 10 | 10 | 8 | 8 | 8 |  |  |  |  |  |  |  |  |  |
| 280 | 10 | 10 | 8 | 8 | 8 |  |  |  |  |  |  |  |  |  |
| 300 | 10 | 10 | 8 | 8 | 8 |  |  |  |  |  |  |  |  |  |

## DISTRIBUTION UNIFORMITY

Formula for finding low quarter distribution uniformity

$$
\text { DUlq }=\frac{\text { LQavg }}{\text { Vavg }}
$$

## WHERE

DUlq = Low Quarter Distribution Uniformity
LQavg = Average Catch in Lower Ouarter
Vavg = Average Catch Overall

## DRIP IRRIGATION

Three Simple Steps to Getting Started
Step 1: Determine the water needs of plant. Consult the experts from which you
purchased your plant materials, or locate the evapotranspiration (ET) data online.
Step 2: Calculate the drip application rate.
Application Rate (in/hr) =
GPH x 1.604
irrigated area (in square feet)

## Step 3: Adjust the run times.

| Run Time <br> (in minutes) |
| :--- |$\quad$| in. of water required |
| :---: |
| application rate |$\times 60$

## CONVERSION FORMULAS

## $\mathbf{V}=\mathrm{W} / \mathrm{A} \quad \mathrm{A}=\mathrm{W} / \mathrm{V} \quad \mathrm{V} \times \mathrm{A}=\mathrm{W}$

## $\mathbf{V}=$ Voltage

$\mathrm{A}=$ Amperage
$\mathrm{W}=$ Watts

## HARDSCAPE

Sand Setting Bed and Compacted Aggregate Base Material
Calculation Chart

|  | TONS | YDS ${ }^{3}$ | TONS | YDS ${ }^{3}$ | TONS | YDS ${ }^{3}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SQUARE FEET | 100 |  | 150 |  | 200 |  |
| 1" Sand Setting Bed | 0.45 | 0.3 | 0.75 | 0.5 | 0.9 | 0.6 |
| 4" Compacted Aggregate Base | 2.3 | 1.3 | 3.5 | 2.0 | 4.6 | 2.6 |
| $6^{\text {" }}$ Compacted Aggregate Base | 3.6 | 2.0 | 5.4 | 3.0 | 7.2 | 4.0 |
| 12" Compacted Aggregate Base | 7.2 | 4.0 | 10.8 | 6.0 | 14.4 | 8.0 |
| Calculations are approximate. Ouontities may vary depending upon materiol density and moisture content. |  |  |  |  |  |  |

## FORMULAS

| Area of a rectangle | length $\times$ width |
| :--- | :--- |
| Area of a triangle | $1 / 2$ (base $\times$ height) |
| Area of a circle | 3.14 (radius $\times$ radius) |
| Cubic feet | length $\times$ width $\times$ height |
|  | $(27$ cubic feet $=1$ yard) |

## VOLTAGE DROP

Cable Constant Voltage Drop Formulas
(run length in feet)

## 8 GAUGE

| $\frac{\text { watts } \times \text { run length } \times 2}{18,960}=$ Voltage Drop |
| :--- |
| $\mathbf{1 0}$ GAUGE |
| $\frac{\text { watts } \times \text { run length } \times 2}{11,920}=$ Voltage Drop |
| $\mathbf{1 2}$ GAUGE |
| $\frac{\text { watts } \times \text { run length } \times 2}{7,500}=$ Voltage Drop |
| $\mathbf{1 6 ~ G A U G E ~}$ |
| $\frac{\text { watts } \times \text { run length } \times 2}{2,200}=$ Voltage Drop |

